An Overview of Bulk Parametrization and Remote Sensing of Latent Heat Flux in the Tropical Ocean

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1. INTRODUCTION

The only practical way of determining large-scale air-sea exchanges in momentum, heat and moisture is through the bulk formulae which link the microscale turbulent transfer to macroscale parameters measured routinely. The coefficients used in these formulae were derived and verified with observations taken in moderate wind conditions (4-15 m/s) under near neutral condition. Over large areas in the tropical Pacific, the mean wind is weak (< 3 m/s) and the sea-air humidity difference reaches above 7 g/kg (e.g., Hsiung 1986). The moisture induced buoyancy destabilizes the atmosphere and increases evaporation. The characteristics of the coefficients under these conditions will be discussed

Except near coastal area and in major shipping lanes, meteorological reports are sparse in the tropical ocean. *In situ* measurements are not adequate to delineate the temporal and spatial variabilities of the fluxes. Spaceborne sensors provide repeated and uniform coverage. A method of computing the moisture flux using spaceborne sensors will be described and examples of scientific application will be presented.

2. FORCED CONVECTION

The bulk parameterization formulae are

$$\tau = \rho C_D U^2 \tag{1a}$$

$$H = \rho c C_H U (T_s - T)$$
(1b)

$$E = \rho C_E U (Q_s - Q)$$
 (1c)

where τ is the wind stress, H is the sensible heat flux, E is the moisture flux, ρ is surface air density, c is the isobaric specific heat. The latent heat flux (LE) is the product of E and the latent heat of vaporization. The measurements required are the sea surface temperature (T_s), the wind speed (U), the temperature (T), and the specific humidity (Q) measured on board ships. The specific humidity at the air-sea interface (Q_s) is generally taken to be the saturation value at T_s and Q can be derived from the dew-point temperature measured. The transfer coefficients (C_D, C_H and C_E) used are generally assumed to be constant and determined by regression of spot measurements (10 min to 1 hr time averages at a fixed location). The coefficients, in theory, depends on the reference height, the stability and surface roughness. Liu et al. (1979) developed a model to account for these variabilites.

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In the model of Liu et al. (1979), which is a physical approach to bulk parameterization, the three non-dimensional profiles based on similarity theory are solved simultaneously. The similarity relations are,

$$U/U_* = 2.5(z/z_0 - \psi_U) = C_D^{-1/2},$$
 (2a)

$$(T - T_s)/T_* = 2.2(z/z_T - \psi_T) = C_D^{1/2}C_H^{-1},$$
 (2b)

$$(Q - Q_s)/Q_* = 2.2(z/z_Q - \psi_Q) = C_D^{1/2}C_E^{-1}.$$
 (2c)

By definition, U*, T*, Q* are function of τ , H, and E. The ψ_U , ψ_T , and ψ_Q are function of the stability parameter (ζ) and can be expressed in terms of the three fluxes. The lower boundary parameters z_o , z_T , and z_Q are functions of τ and fluid properties. The three unknowns τ , H, and E can be determined by solving the three implicit equations. This method is similar to that used by Deardorff (1968) to account for the effects of stability on the values of the transfer coefficients and is equivalent to using (1) with variable coefficients.



Fig.1 Laboratory measurements of the vertical profiles of (A) velocity and (B) temperature, (from Liu, 1978).

Fig.2 Variation of the roughness parameter in pipe flow (A) and at the sea-air interface (B), (from Liu, 1978).

Under neutral stability ($\Psi_U=\Psi_T=\Psi_Q=0$), the variabilities of the coefficients are governed by the variabilities of z_0 , z_T , and z_Q . The three parameters reflect the transport processes near the surface. The velocity and and temperature distributions measured in smooth channels by Reichardt (1940) and Deissler & Eian (1952) are shown in Fig. 1. Away from the surface, the flow is turbulent and the measurements follow a logarithmic law. Near the surface, viscosity and conductivity become important and the profiles agree with the postulation based on a surface renewal model by Liu et al. (1979). The imagery height at which the U-U_s=0 along the extrapolation of the logarithmic profile is z_0 . The interpretation of z_T and z_Q are the same except for temperature and specific humidity. Schlichting (1968) suggested that a surface is aerodynamically rough when the roughness elements penetrate the viscous sublayer and it is smooth if the sublayer covers the roughness elements. The scaling depth of the sublayer is v/U*, where v is the kinematic viscosity. Alternatively, rough flow can be viewed as the state when the local velocity scale and the characteristic scale of the roughness elements, ξ , combined to form a roughness Reynolds Number $(\xi U_*/v)$ that exceed a critical value. The velocity measurements in pipe flow by Nikuradse (1933) are shown in Fig. 2A. ξ is the actual mean diameter of the the sand-grains used as roughness elements. The measurements of Kondo (1975) at an air-sea interface are shown in Fig. 2B and ξ is the square root of the integral of the one dimensional wave spectrum between two selected frequencies. In smooth flow, $\xi \ll v/U_*$, momentum is mainly transported by viscosity, z_0 is proportional to v/U_{*}, and, therefore, C_D increases with decreasing U_{*}. In rough flow, $\xi > v/U_*$, momentum is mainly transported by pressure force on the roughness element and the flow is independent of v, and z_0 is proportional to ξ . In the case of a rough sea surface, ξ increases with wind and, therefore, C_D increases with wind. Charnock (1955) postulated that z_0 is proportional to U*²/g where g is the acceleration due to gravity.

When the interface is smooth, momentum, heat and water vapor are all transported by molecular processes near the interface and the variations of C_D , C_H , and C_E should share the same characteristics, i.e., increases with decreasing winds. When the roughness of the surface increases, turbulent transport is facilitated and the transfer coefficients increase with wind speed. While momentum can be transported by pressure forces on the roughness elements independent of viscosity, the slow molecular diffusion is the only process which transport heat and mass at the interface. Increase in roughness increases the sheltering effect and the fluid stays longer in contact with the surface before turbulence carries it away. The opposing effects on the C_E is shown in Fig. 3. The thick curve represents C_E at neutral stability from the model of Liu et al. (1979). At low wind speed, it decreases with increasing wind speed, having the characteristics of smooth flow described above. The behavior of C_E at low winds was recently supported by the measurements of Bradley et al. (1989) in the Brismack Sea. As the wind speed increases and the surface becomes rough, the opposing effects of increase stirring and sheltering balance out and the C_E remains rather constant at 1.3x10⁻³ in good agreement the empirical values (shown as dashed lines) by Anderson and Smith (1981) (A&S) and Large and Pond (L&P). The value given by Bunker (1976) (B), however, increases with wind speed, following the characteristics of C_D.

In (2), ψ_U , ψ_T , and ψ_Q are functions of the stability parameter ($\zeta = z/L$), where z is the height and L is the Monin-Obukhov length. The parameter is the ratio of turbulence production by buoyancy to those by shear. Assuming $C_D = C_H = C_Q = C$, it can be approximated (Deardorff, 1968) by

$$\zeta \cong \frac{\text{kgz} (\Delta T + 0.619 \Delta Q)}{\sqrt{C} \theta U^2}$$
(3a)

where k is the von Karman's constant, $\Delta T = T_s - T$, $\Delta Q = Q_s - Q$, and θ is the average absolute temperature. As the flux-profile relations, initially developed over land, are extended over water, the effects of humidity fluctuation on buoyancy is often overlooked. Bunker (1976), for example, tabulated the values of the transfer coefficients according to classes of U and ΔT but not ΔQ . In the extratropical oceans, the effects of humidity fluctuations may be small compared with the effects of temperature fluctuations. But in the tropical oceans, due to the rapid increase of saturation humidity at high temperature (Clausius-Clapeyron Equation), humidity fluctuations can have significant effects on atmospheric stability and the variability of the transfer coefficient. Fig 4 shows the ratio of ζ / ζ_* where

$$\zeta_* \cong \frac{\operatorname{kgz} \Delta \mathrm{T}}{\sqrt{\mathrm{C}} \, \theta \, \mathrm{U}^2} \tag{3b}$$

at various T_s and two values of ΔT , assuming C=1.3 x10⁻³, U=7 m/s and a relative humidity of 80%. It is obvious that the error for omitting ΔQ can be larger than 50% over warm water (>25°C). In the western tropical Pacific and eastern Indian Ocean, with a typical wind speed of 4 m/s, and a typical sea-air humidity difference of 6 g/kg (Hsiung, 1986), the coefficient is approximately 1.8×10^{-3} as shown in Fig. 3. This will give a latent heat flux approximately 40% higher than the value given by a neutral coefficient of 1.3×10^{-3} . The typical ΔT may be small and the temperature induced buoyancy alone cannot adequately account for the stability effect on C_E.





Fig.3 Variation of the moisture transfer coefficient with wind and sea-air humidity difference computed with model of Liu et al. (1989), with the thick line representing values at neutral stability.

Fig 4. The ratio of the stability parameter including humidity effects to the stability parameter excluding humidity effects as a function of temperature for two cases of sea-air temperature differences (ΔT).

FREE CONVECTION 3.

The bulk formula (1) imply that there is no heat and moisture transfer at zero wind speed which, of course, is not true. Convection caused by buoyancy force as a result of heating or concentration gradient will transport heat and moisture. The similarity profiles (2) are not valid under free convection when buoyancy dominates over shear in turbulence production. In open oceans, free convection is rare and is not well studied. However, there are many studies of free convection of homogeneous fluids, particularly in laboratory Liu (1984) gave a detailed review. Krishnamurti (1973) showed that the circulation in a fluid goes from laminar to fully turbulent as the Raleigh number for temperature (RaT= $\alpha g \Delta T d^3/(\kappa_T v)$ increases. In the definition of Ra_T, α is the coefficient of thermal expansion and κ_T is the thermal conductivity. When the flow is fully turbulent, theoretical and empirical studies suggest that the heat transport is governed by

$$Nu = A Ra_T^{1/3}$$
(4)

where $Nu=Hd/(\rho c \kappa \Delta T)$ is the Nusselt number, and A depends on the Prandtl Number Pr=v/kT. Fig. 5, from Liu (1974), shows the results of an experiment with a deep wellinsulated tank of water under an evaporating free surface Surface heat flux is equated to water heat loss derived from calorimetry. Water surface temperature was measured both by an Barnes PRT-5 radiometer mounted above the tank and by moving a 25 micron diameter resistant film probe across the surface. The bulk temperature was measured by a thermometer. The 110 pairs of data have a correlation coefficients of 0.997 and the linear fit corresponds to a relation $Nu = 0.156 Ra_T$ Eqn (4) can be reduced to



Raleigh Number for temperature (RaT) for natural convection under a free surface (from Liu, 1974)

Fig 6 Comparison of field measurements of heat flux under free convection and values predicted by (6) (from Golitsyn and Grachov, 1988).

300

400 FLUX PREDICTED

500

600 700

100 200 150

$$H = A\rho c \left(\frac{\alpha g \kappa_T^2}{v}\right)^{1/3} \Delta T^{4/3}$$
 (5)

The relation between Q and ΔT is independent of the depth of fluid. For a inhomogeneous fluid like the atmosphere over ocean, (4) can be generalized to include moisture transport,

$$Nu = A \left[Ra_{T} + Ra_{Q} \left(\frac{Pr}{Sc} \right)^{3/2} \right]^{1/3}$$
(6a)

$$Sh = A \left[Ra_Q + Ra_T \left(\frac{Sc}{Pr} \right)^{3/2} \right]^{1/3}$$
(6b)

where Sh=Ed/($\rho\kappa_Q\Delta Q$) is the Sherwood number, Sc=v/ κ_Q is the Schmidt number, κ_Q is the diffusivity of water vapor, Ra_Q= $\beta g\Delta Qd^3/\kappa_Q v$ is the Raleigh number for humidity, and β is the expansion coefficient due to water vapor. The heat and moisture fluxes can be reduced to functions of ΔT and ΔQ . Fig. 6, from Golitsyn and Garchov (1986), compared field measurements of heat and moisture fluxes to those predicted by (6).

Wyngaard et al. (1971) recognized that the similarity theory breaks down when there is no mean wind and introduce a free convection scale for the atmospheric mixed layer with depth d

$$U_{f} = \left(\frac{\alpha g dH}{c\rho}\right)^{1/3}$$
(7)

and Businger (1973) postulated that convection will induce local surface friction velocity, U* and $U*/U_f$ is a decreasing function of d/z_o . Assuming

$$\frac{U^*}{U_f} \propto \left(\frac{d}{z_o}\right)^{1/3} \tag{8}$$

and that the resident time scale of the fluid at the surface is equal to the Kolmogorov time scale, Liu et al. (1979) derived (4) from (8). Schuman (1988) suggested that (4) is applicable only to smooth flow. In rough flow, he suggested

$$Nu = A RaT^{1/2}$$
(10)

Under free convection conditions, the flow is always smooth over the ocean. The independence of heat flux from any depth scale, as in (6), remains to be vigorously tested.

4. LATENT HEAT FLUX FROM SATELLITE DATA

Of the three parameters required to compute LE, spaceborne sensors can measure T_s and U, but cannot measure Q. It was found that at the monthly time scale, atmospheric water has a single dominant mode of variability and Q can be derived from the columnar

water vapor (W) measured by microwave radiometers. A statistical Q-W relation was established using 17 years of radiosonde reports from mid-ocean meteorological stations (Liu, 1986). This relation was found to be adequate in describing the seasonal and interannual variations over global oceans except in high latitudes during summer, with accuracy estimated to be 0.4-0.8 g/kg. With this relation, monthly fields of LE from 1980 to 1983 in the tropical Pacific were computed using data from Nimbus/SMMR. In comparison with monthly data from equatorial moorings and atolls, the scatters were found to be 0.6 m/s in U, 0.8°C in T_s and 0.4 g/kg in Q. The random error in LE is estimated to be 26 W/m² (Liu, 1988). The errors for T_s and LE were likely to be overestimated since a 200x200 km satellite average was compared with a spot measurement in an area of very large meridional gradient.

Fig. 7 shows the time-longitude distribution of T_s , U, W, and LE centered on the equator between 90°W and the date-line. The 1982-83 ENSO episode is envisioned as an apparent eastward migration of the warm water pool marked by the 28°C isotherm starting in June 1982. This results in a reverse of zonal T_s gradient near the date-line. The organized deep convection marked by high W also moves east from the date-line starting June 1982, leaving dry air behind. The seasonal cycle of U is disrupted by the eastward migration of low wind center representing surface convergence associated with the organized convection at the eastern terminal of anomalous westerlies. During April 1983, zonal belts of high T_s , high W and low U stretch across the entire equatorial Pacific. Detailed evolution of these three parameters during the episode is described in Liu (1989a). Despite the warm water, LE is below normal due mainly to the low U near the convergence center. The annual October high does not reach the expected level.



Fig.7 Time-longitude variation, centered on the equator, of (A) sea surface temperature, (B) surface wind speed, (C) columnar water vapor, and (D) latent heat flux. The intervals between isolines are 1°C, 1m/s, 0.5 g/cm², and 25 W/m² respectively.

The change of heat storage in the upper ocean is governed by the balance of heat gain from the surface and the loss through ocean dynamics. Fig. 8A shows the distribution of the contemporary correlation coefficient, at 2° latitude by 2° longitude grids, between LE and the time rate of change of sea surface temperature $(\partial T_s/\partial t)$ for the period between February 1980 and September 1983, including an intense El Nino and Southern Oscillation episode. The gradient of the linear regression for three consecutive months of T_s is used to represent $\partial T_s / \partial t$. The 44 months of LE and $\partial T_s / \partial t$ fields were reconstructed from the first three empirical orthogonal functions accounting for 60% and 83% of the variance respectively. The low correlation in the near equatorial regions (left) is due the cloud and insolation variabilities in areas of organized convection and surface convergence (e.g., ITCZ) and due to ocean upwelling (along the equator). Off phase moisture variation is likely to be cause of low correlation at 20°N. Outside of these regions, the correlations are significant, indicating dominant influence of surface latent heat flux in upper ocean heat balance. By adding the surface shortwave radiation derived from observations from the VISSR (Visible Infrared Spin Scan Radiometer) (Liu and Gautier, 1989) to the latent heat flux, the area of low correlation is concentrated in a narrow belt around the equator (Fig. 8B) showing that in this equatorial wave guide, ocean dynamics plays a dominant role.



Fig. 8 Contemporary correlation coefficient between time rate of change of sea surface temperature and (A) latent heat flux (top), and (B) net heat flux (bottom). Solid isolines have 0.2 intervals.

135W

175W

155W

115W

95W

520

5. CONCLUSION

 C_E is constant only as a crude approximation. Most values used in the past led to underestimation of E in the western tropical Pacific (where winds are very light) because they do not account for the smooth flow characteristic of increasing values with decreasing winds and they neglect the moisture-induced instability. A scheme for parameterization under free convection is also described which still needs further validation. Inhomogeneous and non-stationary conditions, related to thermal plumes or convection, are not addressed and required more studies and scrutiny.

A method of estimating E with observations from spaceborne microwave is described. Application has been confined to monthly means but extension of the technique to higher temporal frequencies is being explored (Liu, 1989b). Combination of LE with surface shortwave radiation demonstrated the ocean's response to surface thermal forcing.

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