

# Examination of the Difference between Radiative and Aerodynamic Surface Temperatures over Sparsely Vegetated Surfaces

### A. Chehbouni,<sup>\*</sup> D. Lo Seen,<sup>†,‡</sup> E. G. Njoku,<sup>†</sup> and B. M. Monteny<sup>\*</sup>

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m A}$  four-layer hydrologic model, coupled to a vegetation growth model, has been used to investigate the differences between aerodynamic surface temperature and radiative surface temperature over sparsely vegetated surface. The rationale for the coupling of the two models was to assess the dependency of these differences on changing surface conditions (i.e., growing vegetation). A simulation was carried out for a 3-month period corresponding to a typical growth seasonal cycle of an herbaceous canopy in the Sahel region of West Africa (Goutorbe et al., 1993). The results showed that the ratio of radiative-aerodynamic temperature difference to radiative-air temperature difference was constant for a given day. However, the seasonal trend of this ratio was changing with respect to the leaf area index (LAI). A parameterization involving radiative surface temperature, air temperature, and LAI was then developed to estimate aerodynamic-air temperature gradient, and thus sensible heat flux. This parameterization was validated using data collected over herbaceous site during the Hapex-Sahel experiment. This approach was further advanced by using a radiative transfer model in conjunction with the above models to simulate the temporal behavior of surface reflectances in the visible and the near-infrared spectral bands. The result showed that sensible heat flux can be fairly accurately estimated by combining remotely sensed surface temperature, air temperature, and spectral vegetation

\*ORSTOM, Department Terre-Océan-Atmosphère, Montpellier, France

<sup>‡</sup>Present affiliation: CIRAD, Montpellier, France.

Address correspondence to A. Chehbouni, Hydrology Lab., ORS-TOM, 911 Av. Agropolis, BP 5045, 30042, Montpellier, France.

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REMOTE SENS. ENVIRON. 58:177-186 (1996) ©Elsevier Science Inc., 1996 655 Avenue of the Americas, New York, NY 10010 index. The result of this study may represent a great opportunity of using remotely sensed data to estimate spatiotemporal variabilities of surface fluxes in arid and semiarid regions. © Elsevier Science Inc., 1996

#### INTRODUCTION

Thermal infrared remotely sensed surface temperatures are increasingly being used in simple, operational hydrometeorological models to evaluate the spatial variation in the energy balance components over large ares (Jackson, 1985). While this approach has been found to be successful over surfaces with near full canopy cover with unstressed transpiration, its performance has been questioned over sparsely vegetated surfaces.

From a theoretical view point, sensible heat flux should be expressed in terms of aerodynamic surface temperature since it is aerodynamic temperature that determines the loss of sensible heat flux from a surface. Aerodynamic surface temperature was formally defined as the extrapolation of air temperature profile down to an effective height within the canopy at which the vegetation components of sensible and latent heat flux arise, say  $(d + z_h)$ , where  $z_h$  is the roughness length for heat and d is the zero-plane displacement height assumed to be the same for heat and for momentum (Kalma and Jupp, 1990). The formulation of sensible heat flux using this definition of aerodynamic surface temperature requires, however, an additional resistance to the classical log-profile aerodynamic resistance. This additional resistance, which is called the "excess" resistance, is meant to take into account the fact that there is no thermal equivalent of bluff body force. Therefore, the resistance for heat transfer is higher than the corre-

<sup>&</sup>lt;sup>†</sup>Jet Propulsion Laboratory, California Institute of Technology, Pasadena, California, USA

sponding resistance for momentum. The excess resistance has been formulated in terms of  $\ln(z_m/z_h)$  or its equivalent  $kB^{-1}$  parameter (Chamberlain, 1968), where  $z_m$  is the roughness length for momentum transfer, which is situated at a lower level than  $z_h$ . Currently reported values of  $kB^{-1}$  range between 2 and 10 (Brutseart, 1982). While the roughness length for momentum  $(z_m)$  can be derived from the similarity theory or as a fraction of the canopy height, the estimation of the roughness length for heat  $(z_h)$  is not trivial, especially over sparsely vegetated surfaces. The idea suggested by Monteith in 1963 (cited by Troufleau et al., 1996) was to consider that the exchange of heat and moisture between the surface and the atmosphere takes place at an effective level located at the same height as the effective sink of momentum, that is, level  $d + z_m$ , which corresponds to the level where the logarithmic profile takes its surface value. Then a new aerodynamic temperature was defined as the extrapolation of air temperature profile down to this level. It is confusing that no distinction has been made in the literature between the two expressions of aerodynamic surface temperature. For consistent terminology, one may suggest that the temperature defined at level  $d + z_h$  could be "convective" aerodynamic temperature and that defined at level  $d + z_m$ , momentum aerodynamic temperature. In this study, however, we have solely addressed the case of momentum aerodynamic temperature, and have termed it aerodynamic temperature in the remaining part of the article.

Since aerodynamic temperature cannot be directly measured, it is often replaced by radiative temperature in the formulation of sensible heat flux. The problem is that the derivation of exchange coefficient from Monin– Obukhov similarity theory does not apply when the surface radiative temperature is used instead of aerodynamic temperature in the surface heat flux formulation (Sun and Mahrt, 1995). Under dense canopy, the difference between aerodynamic and radiative surface temperatures is very small, which leads to small errors in heat flux prediction. Over sparsely vegetated surfaces, however, the difference can exceed 10°C, as a result sensible heat flux can be largely overestimated.

Three different approaches for using remote sensing of surface temperature to estimate sensible heat flux over sparsely vegetated surfaces have been suggested in the literature. The first approach is to substitute radiative surface temperature for aerodynamic surface temperature and to add supplementary resistance to the aerodynamic resistance (see Lhomme et al., 1996). Kustas et al. (1989) suggested that this resistance can be formulated empirically as a function of wind speed and surface-air temperature gradient, that is, as  $(kB^{-1} = au (T_r - T_a)$ , where u is the wind speed,  $T_a$  is air temperature, and the coefficient a is an empirical factor that was found to be 0.17 from observations of sparse

vegetation in California and 0.11 for data from Arizona (Kustas et al., 1989; Moran et al., 1994). It must be emphasized, however, that this resistance should not be called  $kB^{-1}$ ; this may induce a confusion between radiative and convective processes. The second approach is to determine a new stability function or define a radiometric exchange coefficient (Sun and Mahrt, 1995) that allowed accurate predictions of heat flux when radiative surface temperature is used. The third approach consists of formulating a relationship between aerodynamic and radiative surface temperature (Brutsaert, 1982). This is a very difficult task since  $T_r$  is a function of radiative and kinetic temperature of the surface, sensor view angle, and surface morphology, while  $T_a$  is a mathematical construct that depends upon the surface radiative and kinetic temperature and on the thermodynamic properties of the air in contact with the surface (Hall et al., 1992).

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In a similar vein, the objective of the present study were: 1) to examine the differences between radiative and aerodynamic temperatures for sparsely vegetated surfaces, and to determine whether a consistent relationship between aerodynamic-air temperature gradient and radiative-air temperature one could be found, and 2) to investigate the possibility of thereby obtaining accurate estimates of sensible heat flux from ancillary meteorological input and remotely sensed data in the visible, NIR, and thermal infrared. The approach adopted for this investigation was based upon the use of a coupled fourlayer hydrological model and a vegetation growth model (LoSeen et al., 1996). The rationale for the coupling of the two models was to assess the differences between aerodynamic and radiative temperatures for changing surface conditions (i.e., growing vegetation).

#### METHODOLOGY

In the following section, brief descriptions of both hydrologic and vegetation growth models are provided, and the coupling procedure is outlined [a complete description and validation of both models can be found in LoSeen et al. (1996)].

#### **Vegetation Growth Model**

This model developed and validated by Mougin et al. (1995) is used to simulate the seasonal cycle of a herbaceous canopy in the Sahel. For a given day of the season, the total aboveground biomass  $B_r$  is divided into three components: green biomass  $B_c$ , standing dead biomass  $B_p$ , and littér biomass  $B_L$  as

$$B_{\rm T}(t) = B_{\rm C}(t) + B_{\rm D}(t) + B_{\rm L}(t) . \tag{1}$$

The temporal variation of the different biomass components is determined by the following equations:

$$\frac{dB_c}{dt} = P_g - R_t - S, \qquad (2)$$

$$\frac{dB_{\nu}}{dt} = S - L, \qquad (3)$$

$$\frac{dB_{L}}{dt} = L - D, \qquad (4)$$

where  $P_g$  is the canopy gross photosynthesis,  $R_t$  is the respiration loss, S is the senescence, L is litter production, and D is the litter decomposition. The canopy gross photosynthesis is expressed as

$$P_{g} = PAR \ \varepsilon_{i}\varepsilon_{g}f(\psi_{c})g(T_{c}) , \qquad (5)$$

where PAR is the photosynthetic active radiation,  $\varepsilon_i$  is the PAR interception efficiency, which is related to the green biomass,  $\varepsilon_g$  is a conversion factor that can be considered as the growth efficiency in the absence of water stress,  $f(\psi_p)$  and  $g(T_c)$  are functions involving the plant water potential  $(\psi_p)$  and plant temperature  $(T_c)$ . These two parameters are provided by the hydrologic model (see below). The total respiration is parameterized as

$$R_t = P_g [1 - Y_c (1 - pr)] + m Y_c B_c , \qquad (6)$$

where  $Y_c$  is the construction growth conversion efficiency that is the ratio of the carbon mass incorporated into new tissues to the total mass of carbon used, m is the maintenance coefficient, and pr is the ratio between photorespiration and the gross photosynthesis. The senescence S is assumed to be constant until seed maturation, which is assumed to occur at peak biomass, followed by a sharp rise after a certain period of negative carbon budget. S is parameterized as a fraction s of the green biomass as

$$S = sB_c . (7)$$

Similarly, the litter production rate is assumed to be constant until peak biomass. The litter decomposition is simulated to follow environmental conditions and livestock grazing. Finally, canopy parameters (leaf area index, vegetation height, and fractional cover) were derived empirically from the different terms of the biomass [see Mougin et al. (1995) for more details]).

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#### Hydrologic Model

The hydrologic model used in this study to simulate the flows of water and heat in the soil-plant-atmosphere continuum is based on two layer formalism. It is similar in many aspects to other models reported in the literature (e.g., Shuttleworth and Wallace, 1985; Choudhury and Monteith, 1988; Shuttleworth and Gurney, 1990). The soil is represented as a two-layer system, one thin surface layer and one thick layer containing most of the rooting system. The prognostic equations of temperature and moisture in the soil are obtained from the

Table 1. Model Simulations for Temporal Changes in Vegetation Characteristics

DOY	LAI	Vegetation Height (m)	Fraction Cover
214	0.04	0.07	0.07
224	0.08	0.12	0.15
234	0.19	0.21	0.30
244	0.29	0.28	0.40
256	0.45	0.39	0.52
264	0.62	0.47	0.62
274	0.78	0.53	0.70
284	0.90	0.55	0.75

force restore method. The surface is represented by two layers, that is, soil and vegetation. The vegetation is assumed to be a single foliage layer, with negligible heat capacity, more or less shielding the soil (depending on the growth of the vegetation). The model simultaneously solves the energy budget equations at the ground and canopy levels by assuming an appropriate partitioning of the available energy between vegetation and soil. The total surface fluxes are then obtained by summing the component fluxes. In addition to the fluxes, this model allows derivation of the components temperatures used to formulate aerodynamic surface temperature, defined at the same height as the effective sink of momentum, which will be called the original aerodynamic temperature:

$$\dot{T}_{o} = \frac{T_{a}/r_{a} + T_{s}/r_{as} + T_{c}/r_{ac}}{1/r_{a} + 1/r_{as} + 1/r_{ac}},$$
(8)

where  $T_s$  is the temperature of the substrate,  $T_c$  is the temperature of the grass canopy,  $r_a$  is the aerodynamic resistance, calculated between the level of the apparent sink for momentum and the reference height,  $r_{as}$  is the substrate resistance, and  $r_{ac}$  (s  $m^{-1}$ ) is the bulk boundary layer resistance of the grass canopy per unit ground area. Finally, radiative surface temperature is then in-

Figure 1. Differences between radiative and aerodynamic surface temperatures throughout the growing season.





Figures 2a-h. Differences between radiative and air temperatures compared against the differences between radiative and aerodynamic surface temperature for selected days through the growing season.

verted from the total outgoing long-wave radiation using an average surface emissivity. It should be emphasized that because of the nonlinear relation between the radiance and the temperature, surface temperature cannot be obtained as a simple areal average of the temperatures of individual elements of the surface (Chehbouni et al., 1995).

#### **Coupling Procedure**

The procedure used to couple the two models is based on the following steps. First, the vegetation growth model, driven by radiation input, vegetation water status, and temperature  $[\psi_p$  and  $T_c$ ; see Eq. (5)] provides canopy parameters, that is, LAI, and vegetation cover and height. Second, the LAI and vegetation height are used by the hydrologic model in the parameterization of the different resistances and the available energy partitioning. A problem is that the two models operate at different time steps. The hydrological model runs at an hourly time step while the vegetation growth model runs at a daily time step. The daily canopy temperature is therefore obtained by averaging the hourly temperatures. Similarly, daily (cumulative) transpiration  $\langle T \rangle$  is computed from the hourly transpiration rate obtained from the hydrological model. The daily transpiration is then used to estimate the daily vegetation water potential  $\langle \psi_p \rangle$  from the soil-plant-atmosphere model as

$$\langle T \rangle = \sum_{i=1}^{2} \Delta z_{i} \frac{\psi_{s} \langle \theta_{i} \rangle - \langle \psi_{p} \rangle}{R_{si}}, \qquad (9)$$

where  $\langle \theta_i \rangle$  is the daily average of volumetric soil moisture of soil layer *i*, which has a thickness  $\Delta z_i$ ,  $\psi$ , is the total potential energy of the soil water (matric potential plus gravitational potential), and  $R_{si}$  is the sum of plant and soil resistances to water flow.

#### **IMPLEMENTATION AND ANALYSIS**

In this study, meteorological data (precipitation, incoming radiation, air temperature, air humidity, and wind speed) collected at the central East subsite during the HAPEX-Sahel experiment (Monteny et al., 1996) were



Figures 2a-h. Continued.

used to implement the above scheme. As mentioned above, the objective was to investigate the differences between aerodynamic and radiative surface temperatures over partial canopy cover conditions. Thus, this analysis was confined to the part of vegetation cycle in which values of fractional cover ranged from about 5% to 80%, which correspond for grass to values of LAI ranging from about 0.05 to about 0.95 (see Table 1). These conditions occurred from day of the year (DOY) 212 to DOY 288.

In Figure 1, the day time hourly differences (from 8:00 to 17:00 LT) between radiative and aerodynamic temperatures are plotted for a period ranging from DOY 212 to DOY 288. One can see in this figure that the differences between radiative and aerodynamic surface temperatures are of sufficient magnitudes that any attempt to ignore them will necessarily lead to erroneous estimates of sensible heat flux. This actually confirms the results reported by Stewart et al. (1989) and Kustas (1990). It can be also noted that daily as well as seasonal variations of these differences do not present any apparent pattern. This may negate any possibility of deriving aerodynamic surface temperature solely from radiative surface temperature, but our objective here is not to establish a direct relationship between radiative and aerodynamic temperatures.

In Figures 2a-h, day time hourly differences between radiative and air temperatures are plotted against the differences between radiative and aerodynamic surface temperatures, for eight selected days through the growing season (see Table 1). Despite some scatters towards the end of the growing season, the differences between the aerodynamic and radiative surface temperatures show a linear increase (slope) with increasing surface-air temperature gradient. In this regard, Kustas (1990) also found that the deviation of  $T_o$  from  $T_r$  grew as the magnitude of  $T_r$  increased. The slope of the radiative-aerodynamic surface temperature difference with respect to the radiative-air temperature difference is constant for a given day but varies significantly throughout the season.

Since the aerodynamic-air temperature gradient that is required to express sensible heat flux and to correct for the stability, we compute by linear regression the slope ( $\beta$ ) of the  $(T_o - T_a)$  and  $(T_r - T_a)$  gradients for each individual day of the simulation period (from DOY 212 to DOY 288) as

$$\beta = \frac{T_o - T_a}{T_r - T_a}.$$
 (10)

In Figure 3, the multitemporal behavior of the coefficient  $\beta$  through the growing season is compared to the variation of leaf area index (LAI). In spite of some scatter, possibly due to the fact that the intercept in the computation of the regression was set to zero, which was not exactly true under cloudy sky conditions, the general tendency is that the coefficient  $\beta$  decreases in a consistent manner with increasing LAI. It should be noted, however, that this pattern is only relevant under partial cover conditions. Under conditions of fully covered surfaces, the discrimination between aerodynamic and radiative surface temperature is no more pertinent, and thus the coefficient  $\beta$  must ultimately approach the value of 1. This extreme case however is out of the scope of the present study. The fact that the  $\beta$  coefficient exhibits a consistent relationship with the LAI throughout the study period suggests that a mean exists to parameterize  $\beta$  with respect to LAI.

#### **Parameterization Development**

A subdata set made up of 21 points randomly selected from the entire data set (76 days), was used to develop the following relationship between  $\beta$  and LAI:

$$\beta = \frac{1}{\exp(L/(L - LAI)) - 1},\tag{11}$$

where L is an empirical factor that was set by least squares regression to a value of 1.5. The remaining data set (55 days) was then used to test the performance of the above relationship. Figure 4 presents a comparison between original  $\beta$  values (obtained by regression) and those simulated using Eq. (11). In spite of some scatter as discussed previously, the agreement between the data and the simulation is fairly good.

By combining Eq. (10) and (11), aerodynamic-air temperature gradient, which is the gradient required for sensible heat flux formulation, can be expressed in terms of radiative-air temperature one as

$$T_o - T_a = \frac{T_r - T_a}{\exp(L/(L - LAI)) - 1}.$$
 (12)

The formulation in Eq. (12) was then used to express sensible heat flux. Figure 5 presents a cross-plot between the original, hourly based, sensible heat flux obtained by the coupled model (called here the original one) and that formulated using  $T_o - T_a$  from Eq. (12) for the remaining 55 days of the data. It can be seen that this parameterization reproduces fairly accurately the original sensible heat flux. The root mean square error



Figure 3. Comparison between the multitemporal behavior of the coefficient  $\beta$  values and the leaf area index.

(RMSE) between simulated and original sensible heat flux values was about 30 W m<sup>-2</sup>.

To validate the performance of this approach, Bowen ratio-based surface fluxes data collected over the herbaceous subsite during the HAPEX-Sahel experiment were used [see Monteny et al. (1996) for measurements description]. In Figure 6, values of sensible heat flux corresponding to 14:00 LT (which is approximately the AVHRR time overpass in Niger) are compared, for a period of about 60 days, to those simulated using the above approach. Agreement between observed and simulated values are satisfactory, the RMSE was about 43 W m<sup>-2</sup>. The result obtained here suggests that sensible heat flux can be accurately estimated if radiative surface temperature, air temperature, and LAI are known. This is of interest, since  $T_r$  and LAI can be potentially obtained from remote sensing. However, the







Figure 5. Cross-plot between original sensible heat flux (obtained by the coupled models) and that obtained using parameterization in Eq. (12).

relationship derived here may be site-specific since it depends on the fitted L factor.

## Application to Remotely Sensed Spectral Vegetation Index

To investigate the extent to which a remotely sensed spectral vegetation index can be combined with remotely sensed radiative surface temperature to derive accurate values of sensible heat flux over sparsely vegetated surfaces, radiative transfer models were used in conjunction with the coupled models to simulate the multitemporal behavior of surface reflectances in the RED and near-infrared (NIR) regions. The radiative transfer model used in this investigation assumes that the scene reflectance in a given waveband and at any day of the season can be represented by a simple area weighted average of the reflectances of dry biomass, green biomass, and soil (LoSeen et al., 1995). The model

Figure 6. Comparisons between Bowen ratio based sensible heat flux and that obtained using the parameterization in Eq. (12) at 14:00 LT for about 60 days.



of Hapke (1981) has been used to parameterize the soil reflectance. Parameters needed to run this model were obtained from the literature (Jacquemoud et al., 1992). Green and dry canopy reflectances were computed using the SAIL model (Verhoef, 1984; 1985). The main parameters needed to run the SAIL model are LAI, leaf angle distribution (LAD), and leaf optical properties. for this study, a spherical distribution was assumed for the leaves. The leaf optical properties were computed using the PROSPECT model (Jacquemoud and Baret, 1990). Finally, the LAI was given by the vegetation growth model. Surface reflectances in the RED and NIR regions were simulated during the study period (from DOY 212 to DOY 288) using the NOAA-AVHRR spectral and geometrical configurations. Since no direc-" tional correction was performed in this study, data corresponding to large view angle, that is, larger than  $\pm 40^{\circ}$ , were not used. RED and NIR reflectances were used to compute the MSAVI (modified soil adjusted vegetation index) as

$$MSAVI = \frac{RED - NIR}{RED \pm NIR + A} (1 + A), \qquad (13)$$

where A is a self adjusting factor defined to adapt the soil noise correction to the proportion of soil seen by the sensor (Qi et al., 1994). A is given by the expression

$$A = 1 - 2 \frac{\text{NIR} - \text{RED}}{\text{NIR} + \text{RED}} (\text{RED} - 1.06 \text{ NIR}). \quad (14)$$

In this study we have considered MSAVI as the vegetation index to use since it was found to be less sensitive to soil brightness variations including shadows than other spectral vegetation indices (Chehbouni et al., 1994). This is of importance since the contribution of bare soil to scene reflectance is very significant for partially covered surfaces.

In Figure 7, the multitemporal variation of MSAVI is compared to that of the  $\beta$  coefficient. The behavior of MSAVI with respect to  $\beta$  is very similar to that of the LAI (refer to Fig. 3). This is not surprising since the LAI is the major input parameter that drives the SAIL model used to simulate surface reflectances. An interesting feature to note in this figure is that the day to day change in the computed MSAVI is much larger than that of the LAI. This is an artifact, mainly due to the effect of view and sun angle variations in the AVHRR configuration used to compute MSAVI (apparent 9-day cycle). Following the discussion in the previous section, there are two possibilities for obtaining sensible heat flux using radiative surface temperature and MSAVI. One can derive directly a relationship between  $\beta$  coefficient and MSAVI similar to that in Eq. (11), or establish a parameterization between LAI and MSAVI first and then use Eq. (12). The second option was chosen here since LAI can be used elsewhere in the surface flux modeling. Previous studies have indicated



Figure 7. Comparison between the multitemporal behavior of the coefficient  $\beta$  values and the MSAVI.

that a modified Beer's law expression can accurately describe the general relationship between vegetation index and LAI (Asrar et al., 1984; Choudhury et al., 1994). A similar approach to that used to derive Eq. (11) was taken to relate MSAVI to LAI: a part of the data served to calibrate the LAI-MSAVI relationship (the same 21 days mentioned above) and the remaining part to validate it. This leads to a relationship between LAI and MSAVI, which is very similar to that developed by Huete et al. (1985) for cotton data in Arizona:

$$MSAVI = 0.88 - 0.78 EXP(-0.6 LAI).$$
 (15)

Figure 8 presents a comparison between the original sensible heat flux and that obtained by combining the above relation with Eq. (12). It can be seen that the parameterization reproduces fairly accurately the original flux; the RMSE was about 32 W  $m^{-2}$ . This result is almost identical to that shown in Figure 5. This may indicate the goodness of close relationship between LAI and MSAVI, but may also suggest that a part of the noise associated with Eq. (11) might be canceled out with that associated with the view and sun angle effect. The outcome of this study is that there is a real possibility of estimating accurately sensible heat flux from sparsely vegetated surfaces using radiative surface temperature and remotely sensed spectral vegetation index. It is important to remember, however, that the results presented here are for simulated surface reflectances only; further validation with real satellite data under different environmental conditions is needed.

#### DISCUSSION AND CONCLUSION

Recent advances in remote sensing technology allow estimation of land surface temperature from space with reasonable accuracy. Radiative surface temperature can immediately be used in conjunction with ancillary meteorological data for the estimation of regional surface



Figure 8. Cross-plot between original sensible heat flux and that obtained by combining Eqs. (12) and (15).

fluxes. However, it became clear that such method is not reliable over sparsely vegetated surfaces (Hall et al., 1992; Sellers and Hall, 1992). The problem has been that, over partial-cover conditions, convective flux should not be expressed in terms of radiative surface temperature, but in terms of aerodynamic surface temperature. We note here that the relationship between radiative and aerodynamic surface temperature has been a subject of research for more than 10 years. It has been reported the difference between radiative and aerodynamic surface temperature depends on atmospheric stability/unstability and on solar zenith angle, surface soil moisture, and vegetation status.

In this analysis, a hydrologic model coupled with vegetation growth model has been used to investigate the differences between aerodynamic and radiative surface temperatures over partially covered surfaces. One can argue that there is no need for such a coupling to address the above issue. This same analysis can certainly be performed using only the hydrological model. However, it is not realistic for the same vegetation type, to vary for example, the leaf area index while keeping the vegetation height and the fractional cover constant. Thus, the only possibility is to perform an univariate analysis, but it is somehow restrictive.

Our results have shown that the ratio between radiative-air and aerodynamic-air temperature differences is intimately related to LAI. This is actually not surprising since the LAI is pertinent parameter characterizing the vegetation status but is not used in onelayer-based sensible heat flux estimations, whereas it plays a key role in the determination of bulk boundarylayer resistance in the two-layer-based schemes. Thus, LAI should be included in any attempt to derive aerodynamic-air temperature gradient from radiative-air temperature gradient, over sparsely vegetated surfaces (Prévot et al., 1994).

One may argue that the ratio  $\beta$  should also depend on surface soil moisture. Surface soil moisture is certainly a critical parameter that controls the partitioning of available energy at surface into sensible and latent heat flux. However, radiative surface temperature, which represents the signature of an equilibrium of the surface, is directly controlled by surface soil moisture. Therefore, we feel that the dependence of  $\beta$  on soil moisture is through the surface temperature. A parameterization involving radiative surface temperature, air temperature, and LAI has been developed here to formulate sensible heat flux. The simulations showed that this parameterization can be successful in estimating sensible heat flux over a partially vegetated surface. Additionally, the performance of this approach has been verified using Bowen ratio based sensible heat flux, where the RMSE was not very high comparatively to the error associated with the measurements over such complex terrain (Lloyd et al., 1996). The performance of this approach has been also confirmed elsewhere using data taken over shrub and cotton canopies (Chehbouni et al., 1996). Nonetheless further studies are needed to test the generality of Eq. (11), and to investigate how the L parameter changes with vegetation type and structure.

Finally, the radiative transfer model simulations showed that there is a real potential to remotely estimate sensible heat flux. The simplicity of this approach combined with the availability of long term satellite data (i.e., AVHRR) makes it easy to incorporate the approach into energy balance models to investigate spatial and temporal changes in energy fluxes over arid and semiarid lands. However, correction of directional as well as atmospheric effects for both surface reflectances and temperature is needed before this approach can be performed operationally, but this represents one of our future research objectives. We will also investigate the extent to which the L factor in Eq. (11) can be better characterized using multidirectional data. Finally additional field data over different arid surfaces are needed for testing the consistency of the approach.

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